

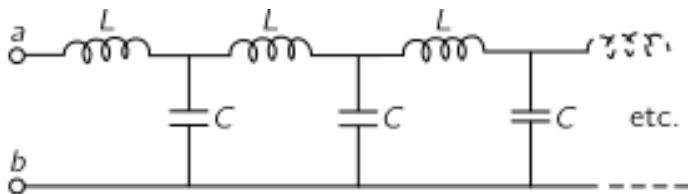
Fractal Alternating Current Ladder Circuits

Loren Anderson and Hannah Davis

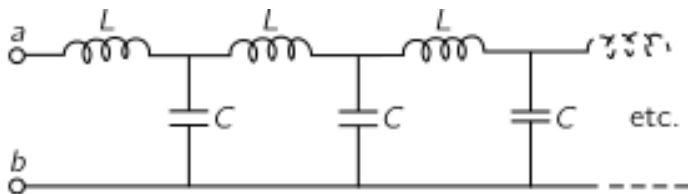
Math REU 2015 at UConn

March 19th, 2016

Infinite Ladder Circuit



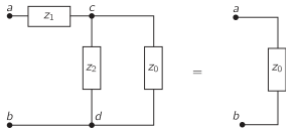
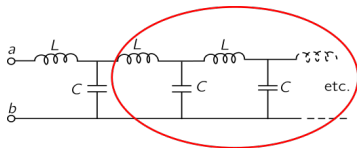
Infinite Ladder Circuit



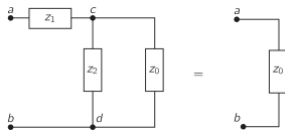
$$z_L = i\omega L$$

$$z_C = \frac{1}{i\omega C}$$

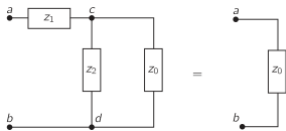
Characteristic Impedance



Characteristic Impedance

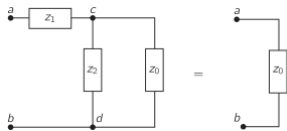


Characteristic Impedance



$$z = \left(\frac{1}{1/(i\omega C)} + \frac{1}{z} \right)^{-1} + (i\omega L)$$

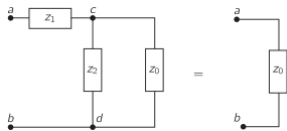
Characteristic Impedance



$$z = \left(\frac{1}{1/(i\omega C)} + \frac{1}{z} \right)^{-1} + (i\omega L)$$

$$z = \frac{1}{2C} \left(i\omega LC + \sqrt{4LC - \omega^2 L^2 C^2} \right)$$

Characteristic Impedance

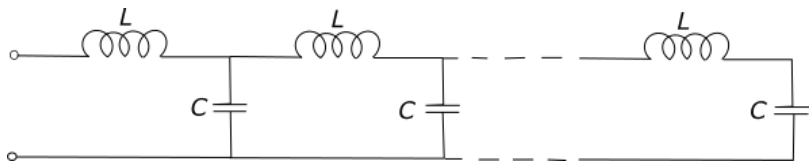


$$z = \left(\frac{1}{1/(i\omega C)} + \frac{1}{z} \right)^{-1} + (i\omega L)$$

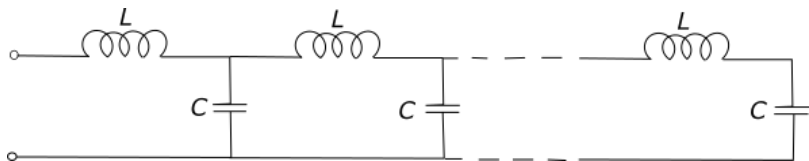
$$z = \frac{1}{2C} \left(i\omega LC + \sqrt{4LC - \omega^2 L^2 C^2} \right)$$

Filter Condition: $\omega^2 LC < 4$.

Finite Approximations



Finite Approximations

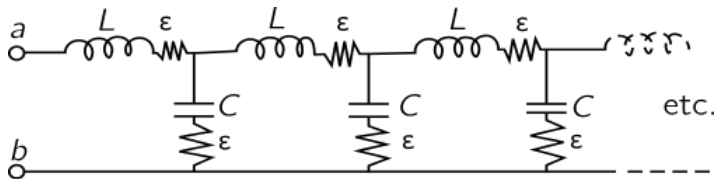


Yoon 2007

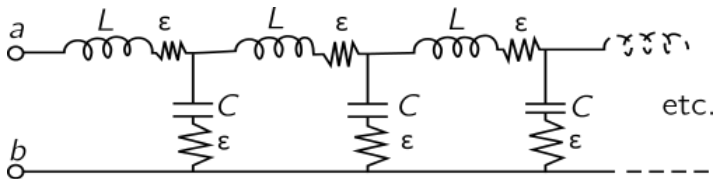
Let z_N be the characteristic impedance of the circuit at the N^{th} stage.

Then $\lim_{N \rightarrow \infty} z_N$ does not exist.

Finite Approximations



Finite Approximations

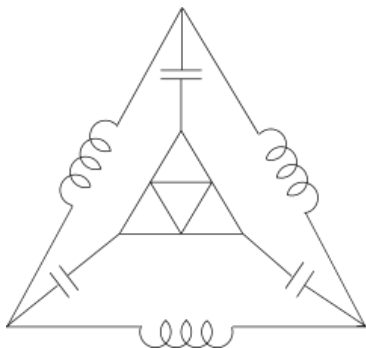


Yoon 2007

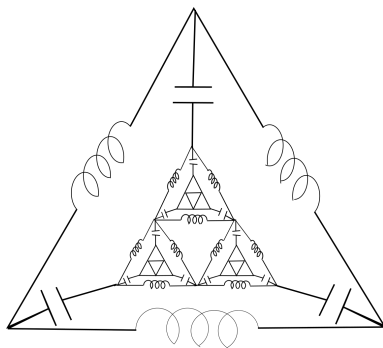
Let $z_{N,\epsilon}$ be the characteristic impedance at the N^{th} stage of construction of the infinite ladder with small real $\epsilon > 0$ added to each impedance. Then,

$$\lim_{\epsilon \rightarrow 0^+} \lim_{N \rightarrow \infty} z_{N,\epsilon} = z = \frac{1}{2C} \left(i\omega LC + \sqrt{4LC - \omega^2 L^2 C^2} \right)$$

Sierpinski Gasket Circuit Construction

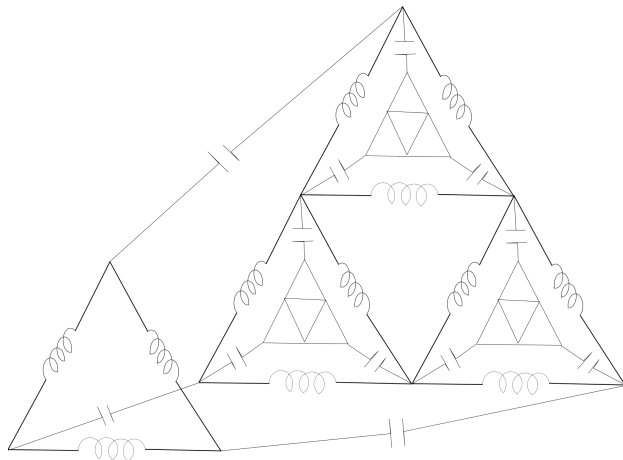


SG circuit level 1



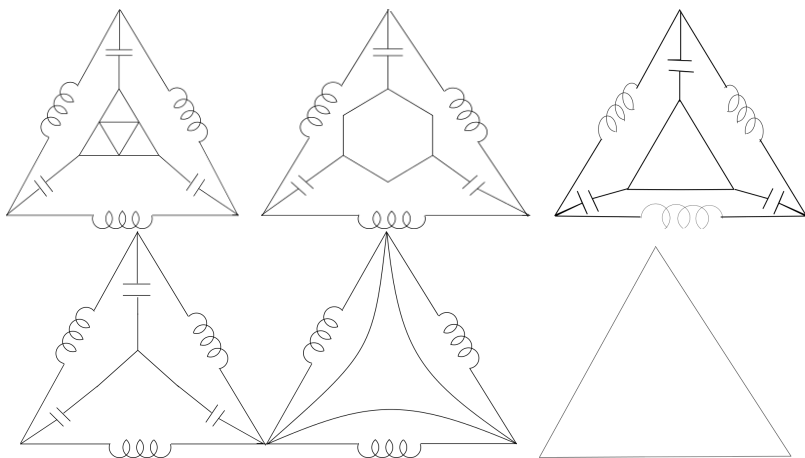
SG circuit level 2

Sierpinski Gasket Circuit Construction



SG circuit level 2

Sierpinski Gasket Circuit Construction



Characteristic Impedance

Theorem 1

If $z_L = i\omega L$ and $z_C = 1/(i\omega C)$, where ω is the AC frequency, then the SG ladder has characteristic impedance

$$z = \frac{1}{10\omega C} \left(2i\omega^2 LC + 9i + \sqrt{144\omega^2 LC - 4(\omega^2 LC)^2 - 81} \right),$$

and is a filter when

$$9(4 - \sqrt{15}) < 2\omega^2 LC < 9(4 + \sqrt{15}).$$

Theorem 2

For finite approximations of the SG ladder,

- i.) $\lim_{N \rightarrow \infty} z_N$ does not exist.

Theorem 2

For finite approximations of the SG ladder,

- i.) $\lim_{N \rightarrow \infty} z_N$ does not exist.
- ii.) $z_{N,\epsilon}$ converges for any $\epsilon > 0$ and

$$\lim_{\epsilon \rightarrow 0^+} \lim_{N \rightarrow \infty} z_{N,\epsilon} = z,$$

the characteristic impedance of the SG ladder.

Harmonic Functions and Extension Matrices

If potentials $f(p_j)$, $j = 0, 1, 2$, are assigned at the outer vertices of the circuit, then energy minimization gives a unique extension to a function f defined on all vertices. This function is harmonic, meaning that for all x ,

$$\Delta f(x) = \sum_{x \sim y} \frac{1}{z_{xy}} (f(x) - f(y)) = 0.$$

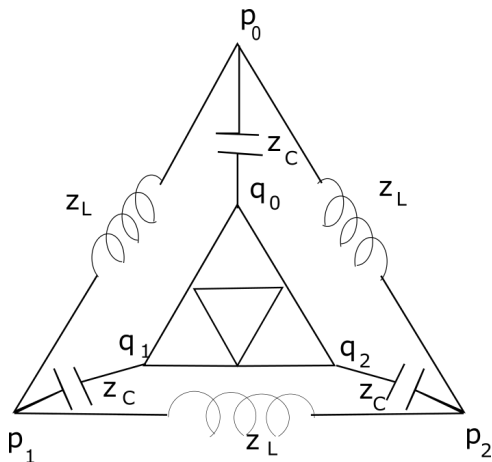
If applied to all points on one level of the graph, this sets up a system of linear equations that allows f to be represented by a product of harmonic extension matrices.

Theorem

The matrix A , below, takes the potentials at the outer points of a SG ladder circuit to those at three outer points of the inner triangle element. Using self-similarity, the potentials at all other points can be determined by iteratively applying A and the known $\frac{1}{5}$ - $\frac{2}{5}$ rule for the Sierpinski Gasket.

$$A = \frac{1}{9z_C + 5z} \begin{bmatrix} 3z_C + 5z & 3z_C & 3z_C \\ 3z_C & 3z_C + 5z & 3z_C \\ 3z_C & 3z_C & 3z_C + 5z \end{bmatrix}.$$

Harmonic Functions and Extension Matrices



Definition

The $\frac{1}{5}$ - $\frac{2}{5}$ rule states that the matrices A_0 , A_1 , and A_2 send the potentials at the outer corners of the level 2 Sierpinski gasket, $f(q_j)$, $j = 0, 1, 2$, to the potentials at the corners of the top, left, and right cells respectively.

$$A_0 = \begin{bmatrix} 1 & 0 & 0 \\ \frac{2}{5} & \frac{2}{5} & \frac{1}{5} \\ \frac{2}{5} & \frac{1}{5} & \frac{2}{5} \end{bmatrix} \quad A_1 = \begin{bmatrix} \frac{2}{5} & \frac{2}{5} & \frac{1}{5} \\ 0 & 1 & 0 \\ \frac{1}{5} & \frac{2}{5} & \frac{2}{5} \end{bmatrix} \quad A_2 = \begin{bmatrix} \frac{2}{5} & \frac{1}{5} & \frac{2}{5} \\ \frac{1}{5} & \frac{2}{5} & \frac{2}{5} \\ 0 & 0 & 1 \end{bmatrix}$$

$$P = IV$$

If the potentials at all points in the circuit are stored in a vector Q , the complex power dissipation is defined by

$$P = (EQ)^T (CEQ) = Q^T E^T CEQ$$

- E is a vertex-edge transference matrix sending the potentials at vertices to the potential differences across edges.
- C is a diagonal conductance matrix sending edge voltage to edge current according to Ohm's law.

Theorem

The operator $D = E^T C E$ that sends potential to total power dissipation on each circuit is invariant under network reduction upon taking the Schur complement.

For the SG circuit with characteristic impedance z , the simplest power dissipation operator is

$$D = \frac{1}{z} \begin{bmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{bmatrix}$$

- [1] R. P. Feynman, R. B. Leighton, and M. Sands, *The Feynman lectures on Physics*, vol. 2. Basic Books, California Institute of Technology, 1965-2013.
- [2] E. Akkermans, J. P. Chen, G. V. Dunne, L. G. Rogers, and A. Teplyaev, *Fractal AC circuits and propagating waves on fractals*. arXiv: 1507.05682.
- [3] S. H. Yoon, *Ladder-type circuits revisited*, vol. 28. Eur. J. Phys., 2007.